

Document No.: NC00.00.00.003
Engineering Report: XFOIL Results For NLF(1)-0215M Airfoil


Applicable paragraphs of airworthiness requirements: N/A

	Name	Signature	Date
Author	-	AP	12.11.2011
Checked	-	-	-
Approved	-	-	-

Rev. No.	Description	Author	Date	Approved
-	Draft	AP	12.11.2011	-

THIS DOCUMENT AND THE TECHNICAL DATA HEREON DISCLOSED ARE PROPRIETARY TO THE ADVANCED DESIGN ALLIANCE (HEREAFTER ADA) AND SHALL NOT BE USED, RELEASED, OR DISCLOSED IN WHOLE OR IN PART WITHOUT EXPRESS WRITTEN PERMISSION FROM ADA.

Advanced Design Alliance (www.adaexp.com)

	Project	Document Name	Document No.	Page
	-	XFOIL Results for NLF(1)-0215M Airfoil	NC00.00.00.003	1

SCOPE


NLF(1)-215M is a modification of a well-known airfoil NLF(1)-215F design for general aviation aircraft. It's intended use is the flap section of a wing. For the aileron section there is supposed to be used an airfoil with less hinge moment.

General

While designing NLF(1)-215M airfoil, several airfoils developed for general aviation applications have been selected for reference and comparison (see a table below). The primary design objectives and constraints for the new airfoil have been set as follows:

- airfoil thickness should not exceed 0.15c;
- blunt trailing edge;
- Cd for cruise is less 0.004;
- the laminar bucket is at least within range of $Cl=0...0.5$;
- Cl_{max} is higher 1.8;
- smooth stall;
- negative Cm is as less as possible to minimize trim drag;
- Cl_{max} must not fall down significantly due leading edge roughness.

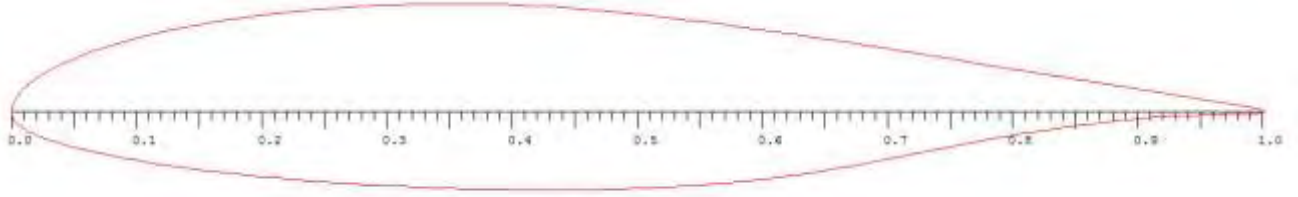
XFOIL 6.96 code has been utilized for the modification. Reynolds numbers of 3e6, 6e6, 9e6 and Mach 0, 0.3, and 0.4 have been analyzed. Rough LE has been simulated by locating the transition from 0.05c at the top surface and 0.05c at the bottom surface.

 ADVANCED DESIGN ALLIANCE ENGINEERING CENTER	Project	Document Name	Document No.	Page
	-	XFOIL Results for NLF(1)-0215M Airfoil	NC00.00.00.003	2


Results

NLF(1)-215M Airfoil Coordinates

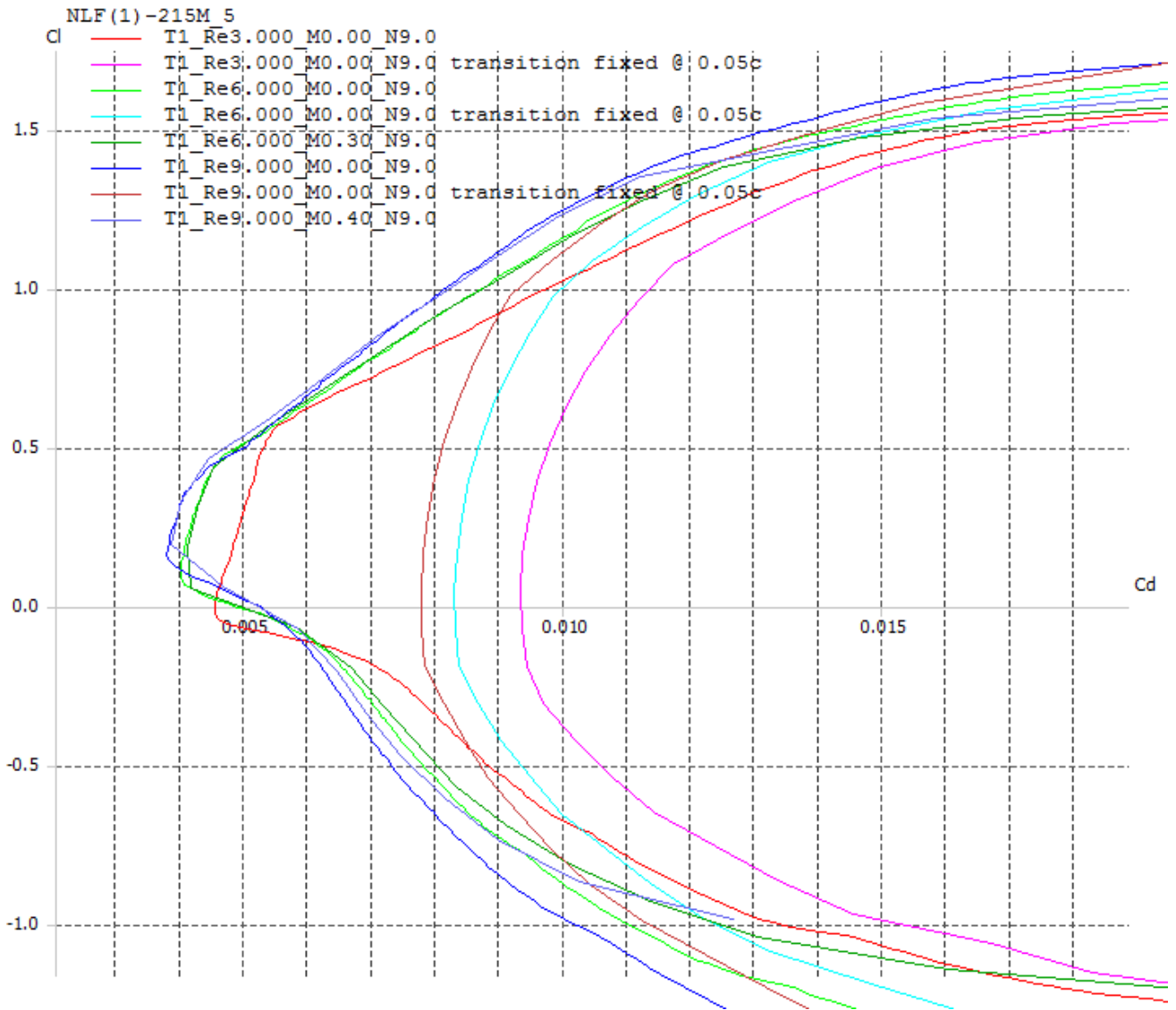
The newly designed airfoil has been re-paneled for 200 points.



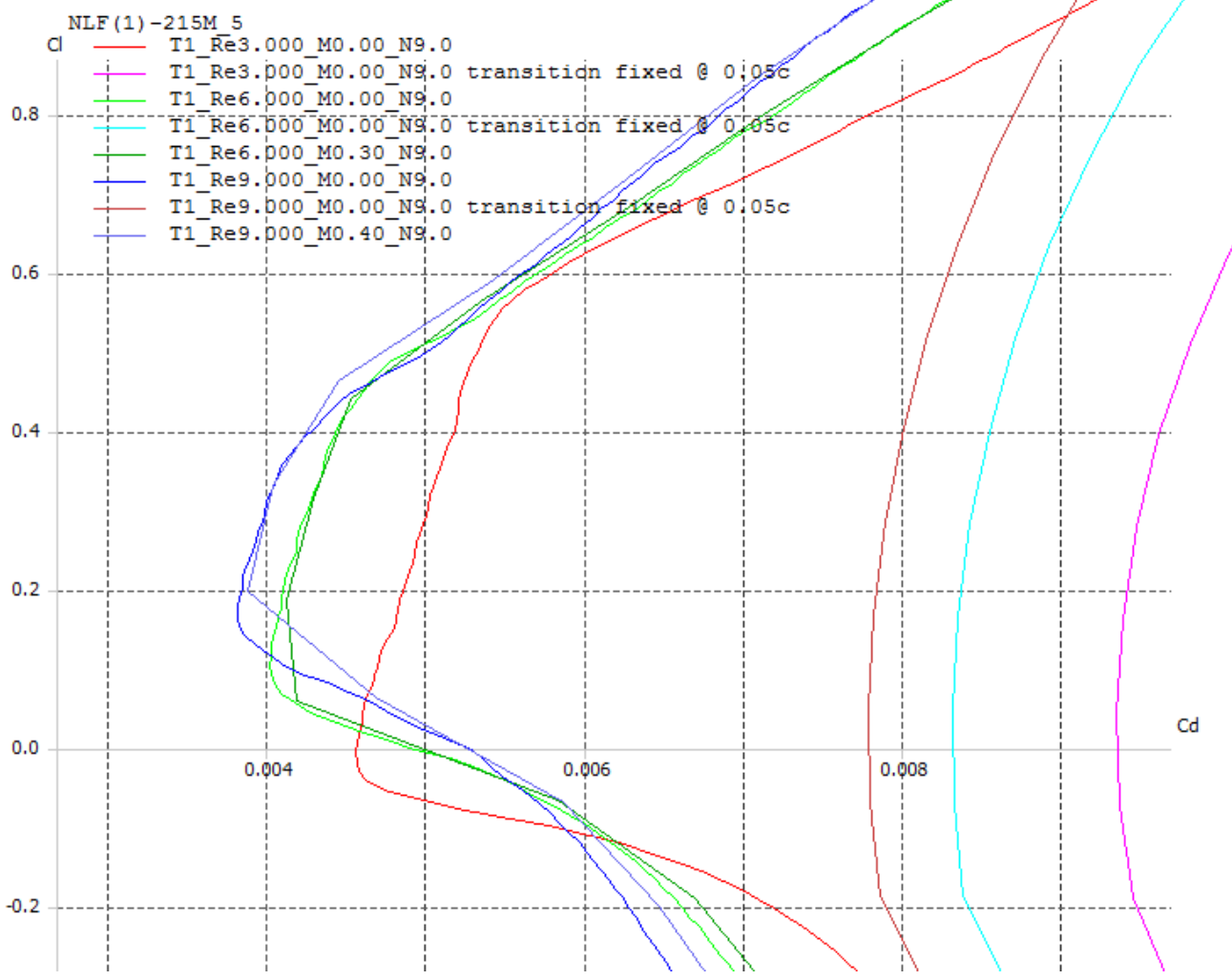
The coordinates have been intentionally removed from this version of the report.

 ADVANCED DESIGN ALLIANCE ENGINEERING CENTER	Project	Document Name	Document No.	Page
	-	XFOIL Results for NLF(1)-0215M Airfoil	NC00.00.00.003	3


Clean Airfoil Analysis

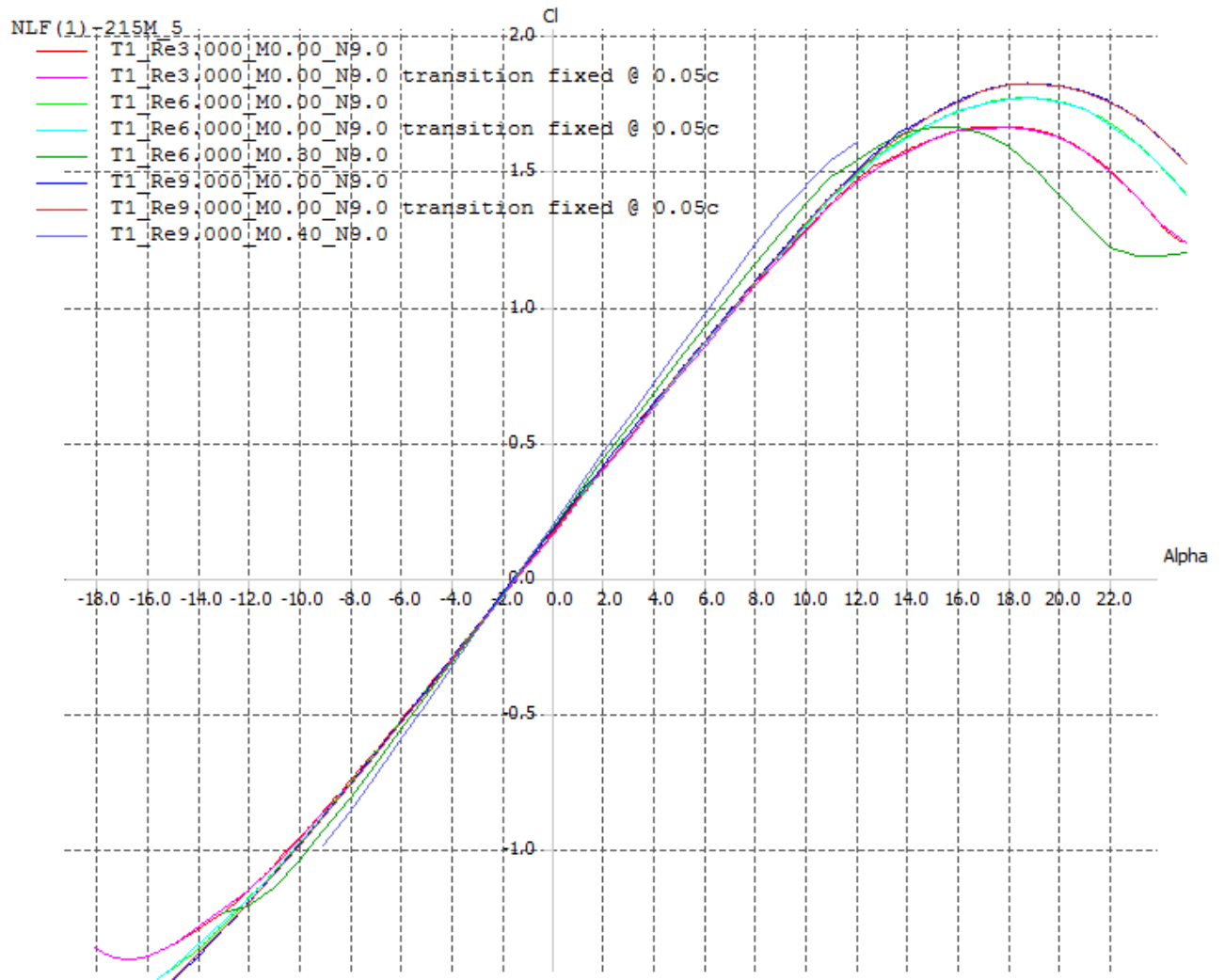


Project	Document Name	Document No.	Page
-	XFOIL Results for NLF(1)-0215M Airfoil	NC00.00.00.003	4




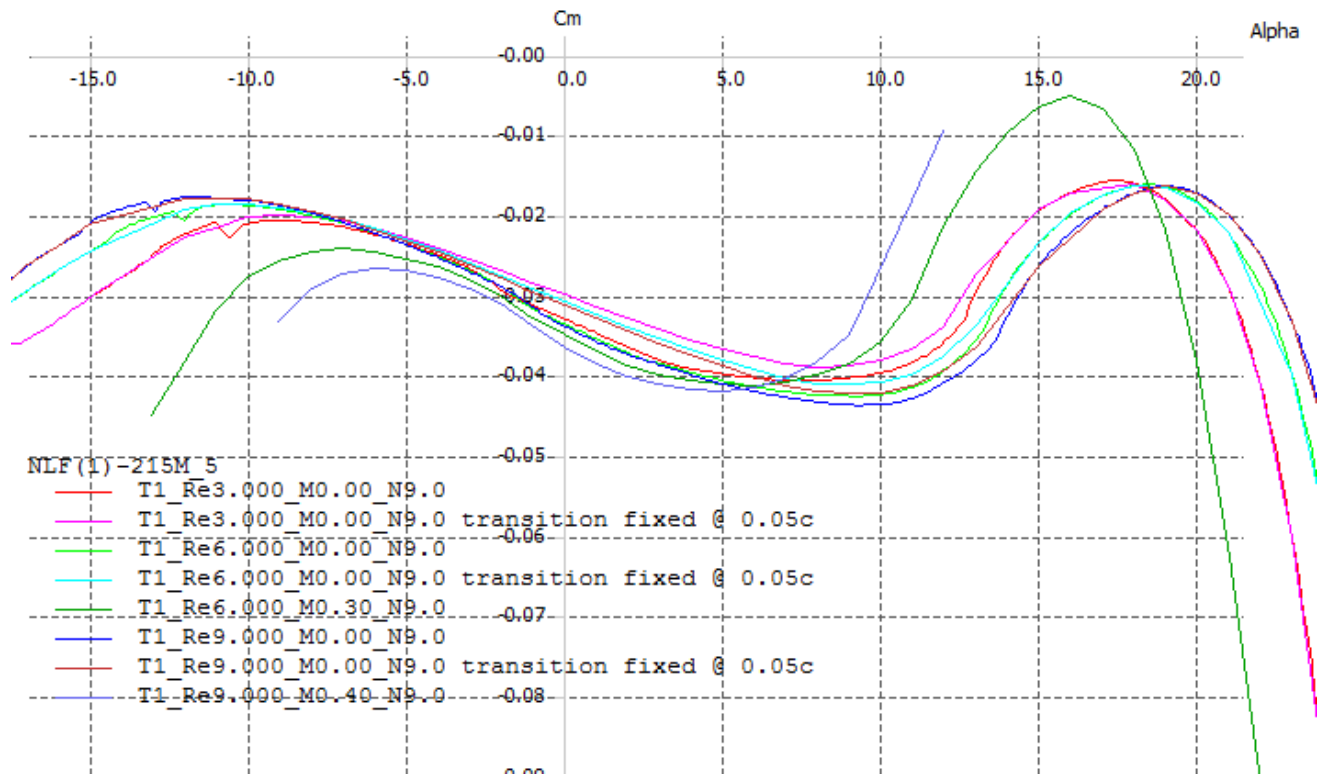
The laminar bucket starts at about $Cl = -0.1$ @ $Re = 3e6$ and ends at about $Cl = 0.6$ @ $Re = 9e6$.


 ADVANCED DESIGN ALLIANCE ENGINEERING CENTER	Project	Document Name	Document No.	Page
	-	XFOIL Results for NLF(1)-0215M Airfoil	NC00.00.00.003	5



The polars with transition fixed show no significant fall of C_{lmax} , if any at all.

	Project	Document Name	Document No.	Page
	-	XFOIL Results for NLF(1)-0215M Airfoil	NC00.00.00.003	6

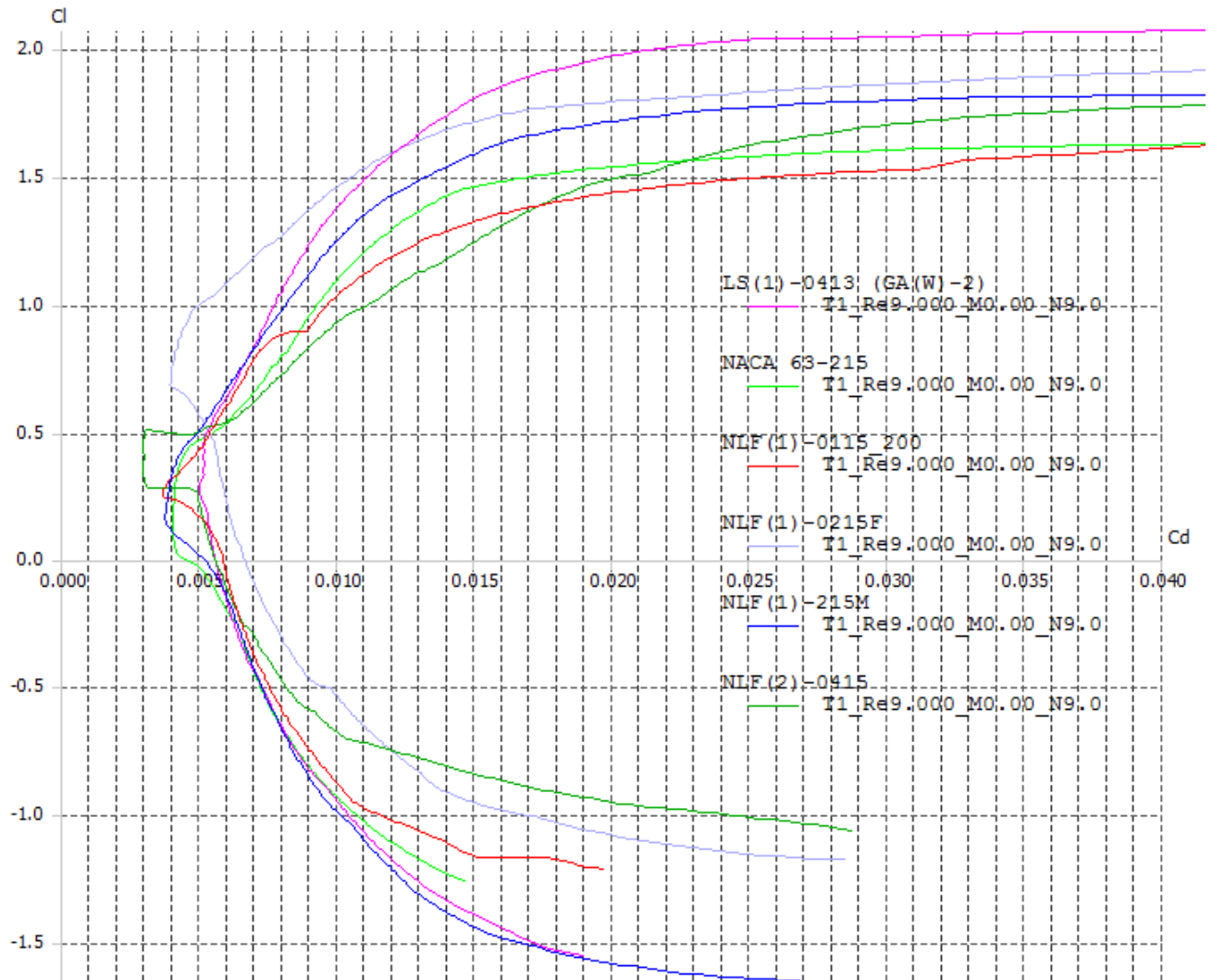


 ADA <small>ADVANCED DESIGN ALLIANCE ENGINEERING CENTER</small>	Project	Document Name	Document No.	Page
	-	XFOIL Results for NLF(1)-0215M Airfoil	NC00.00.00.003	7

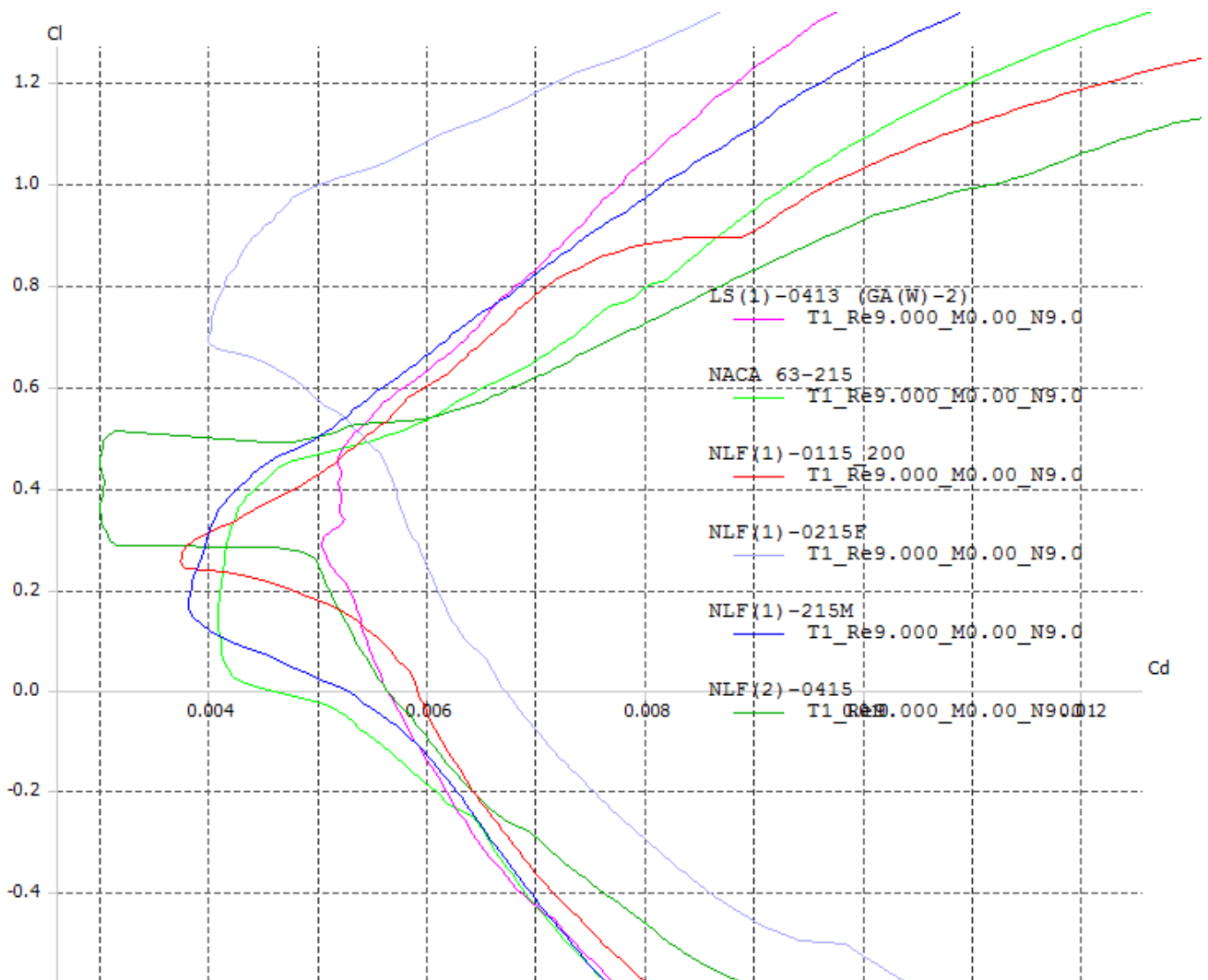
Comparison

For comparison purpose, the selected airfoils have been re-paneled to 200 points each.

$Re=9e6, M=0$



At $C_l=1.0$, except NLF(1)215F due to laminar zone at the range of C_l considered, it's only LS(1)-413 that has less drag, about 0.0077.

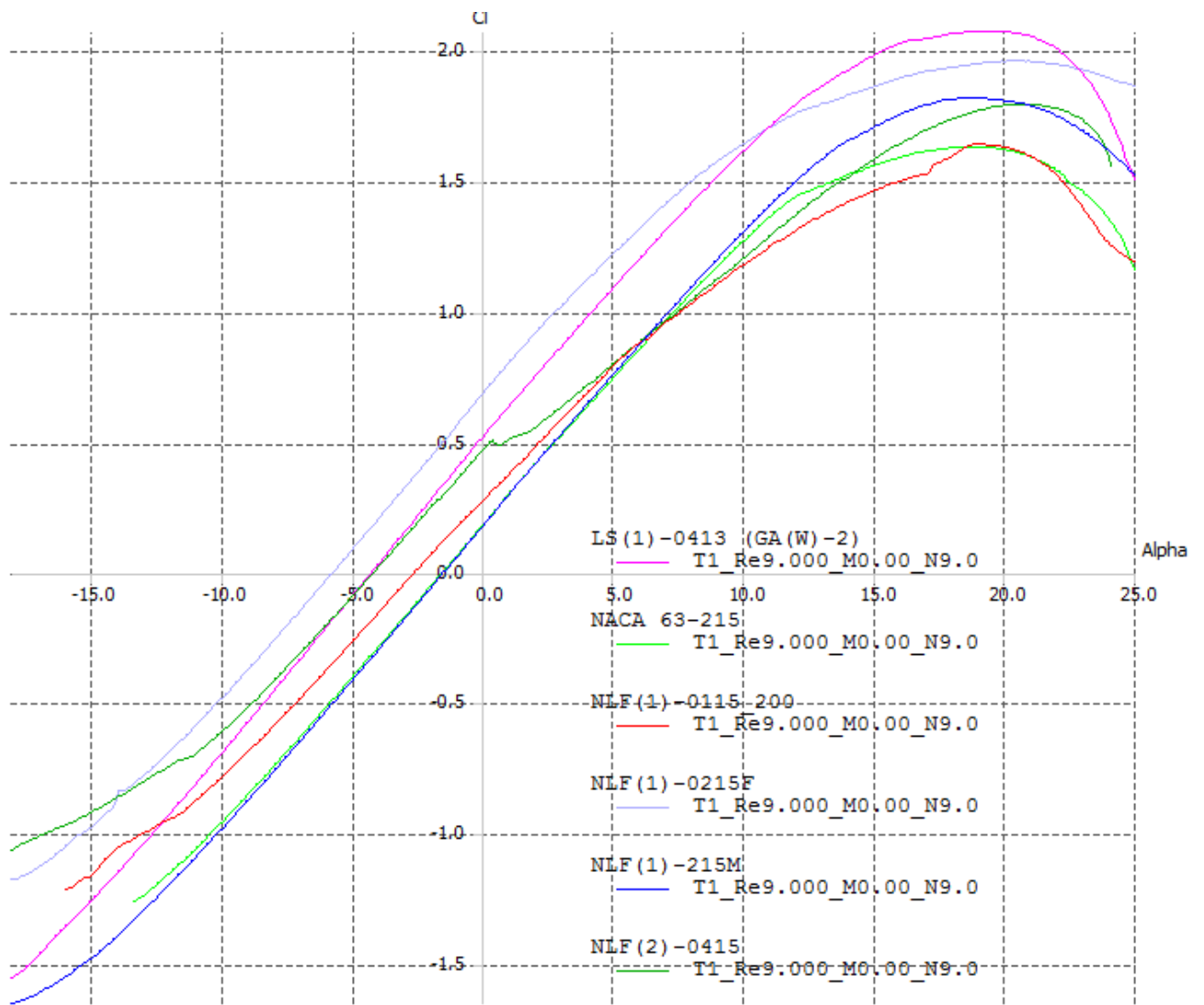


For $C_l=0.5$, where NLF(2)-0415 is laminar and therefore not considered, NLF(1)-215M has minimum $C_{lmin}=0.0049$.


Only NLF(2)-0415 has $C_{dmin}=0.0030$, with about twice as narrow laminar bucket, located at higher C_l (starting from about 0.3), and max thickness located behind $0.5c$. NLF(1)-0115 has the same $C_{dmin}=0.0038$, but very narrow laminar bucket.

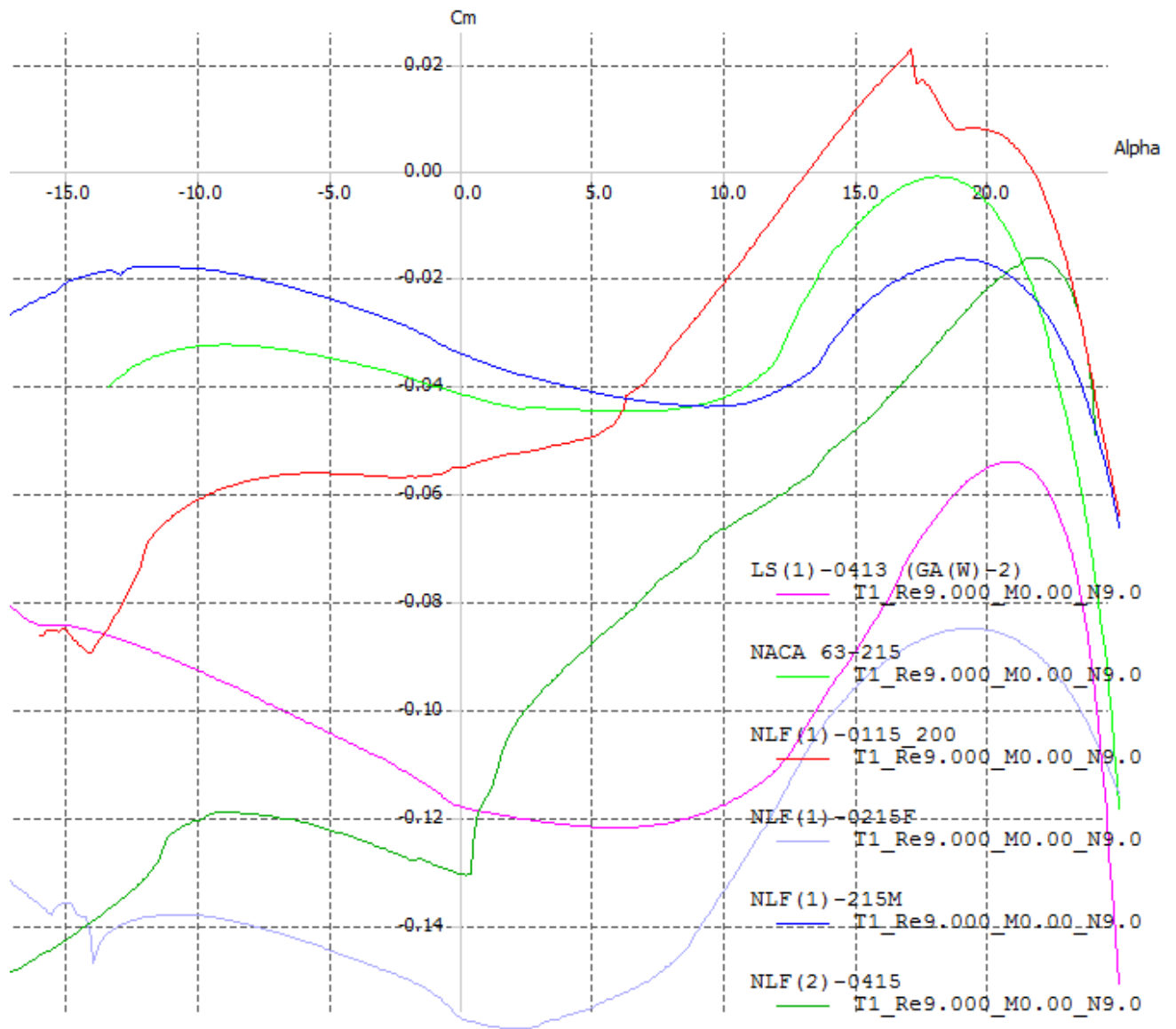
For $C_l=0.2$ of interest for cruise purpose the new airfoil has not competitors. In fact the range with no competitors is about 0.1...0.25. Considering max C_l operating range for a given $C_d=0.004$, for the new airfoil its much wider than for NLF(1)-0115, and about the same as for NLF(2)-0415.

Project	Document Name	Document No.	Page
-	XFOIL Results for NLF(1)-0215M Airfoil	NC00.00.00.003	9




The theoretical $C_{lmax}=1.82$ which is less only for LS(1)-0413 and NLF(1)-215F. A flap is supposed to solve a need in high C_l . The airfoil stalls at 18.6 degrees, while the theoretical range of AOA is wider only for NLF(1)215F (stalls at about 20.5 degrees).

	Project	Document Name	Document No.	Page
	-	XFOIL Results for NLF(1)-0215M Airfoil	NC00.00.00.003	10



NLF(1)-215M positively demonstrates minimal Cm within normal operating range up to AOA=6 degrees, where NLF(1)-0115 starts doing better. However NLF(1)-0115 becomes positive after 13 degrees.

A detailed comparison is presented in Table 1.

	Project	Document Name	Document No.	Page
	-	XFOIL Results for NLF(1)-0215M Airfoil	NC00.00.00.003	11

Flapped Airfoil Analysis

TBD

Flap 10° Configuration

TBD

Flap -10° Configuration

TBD


 ADA ADVANCED DESIGN ALLIANCE ENGINEERING CENTER	Project	Document Name	Document No.	Page
	-	XFOIL Results for NLF(1)-0215M Airfoil	NC00.00.00.003	12

Table 1

	NACA 63-215	LS(1)-0413 (GA(W)-2)	NLF(2)-415	NLF(1)-0215F	NLF(1)-0115	Design Targets	NLF(1)-0215M
Used on Aircraft	Mooney M20TN	Glassair III		Lancair 360			
Vc, km/h	438	505		416			
Re=9e6, M=0							
Thickness, %	15	12.93	15.02	14.99	14.99	<=15	14.76
Cdmin	0.0041	0.0050	0.0030	0.0040	0.0038	<0.004	0.0038
Cl for Cdmin	0.14	0.29	0.45	0.70	0.28	0.20	0.17
Cd @ Cl=0.2	0.0041	0.0053	0.0051	0.0061	0.0048	~0.004	0.0038
Laminar Bucket Clmin	-0.03	N/A	0.27	0.67	0.21	~0	-0.08
Laminar Bucket Clmax	0.5	N/A	0.51	1	0.4	0.51	0.54
Laminar Bucket Width, dCl	0.53	N/A	0.24	0.33	0.19	0.51	0.62
Cd @ Cl=0.5	0.0055	0.0053	0.0031	0.0054	0.0054	0.0040	0.0049
Cd @ Cl=1.0	0.0093	0.0077	0.0110	0.0049	0.0096	0.0069	0.0081
Cl0	0.18	0.53	0.48	0.69	0.28	0.50	0.18
a @ Cl=0	-1.6	-4.3	-4.3	-5.8	-2.7	-3.0	-1.5
a @ Cl=0.2	0.2	-2.6	-2.4	-3.9	-0.8	-1.0	0.2
Clmax	1.63	2.07	1.80	1.97	1.64	1.80	1.82
a @ Clmax	18.5	19.3	20.8	20.5	18.9	19	18.6
Cm0	-0.038	-0.105	-0.123	-0.143	-0.057	-0.030	-0.031
Cm @ a=0	-0.042	-0.117	-0.130	-0.157	-0.055	-0.030	-0.034
Cm @ a=5	-0.044	-0.121	-0.087	-0.155	-0.049	-0.040	-0.041
Cm @ Cl=0.2	-0.042	-0.110	-0.127	-0.146	-0.056	-0.040	-0.034
Cm @ Clmax	-0.008	-0.057	-0.018	-0.086	0.007	-0.008	-0.016


Conclusion

For $Re=9e6$:

- $C_{dmin}=0.0038$ is less than required 0.004;
- the laminar bucket starts at about $Cl=-0.1$ @ $Re=3e6$ and ends at about $Cl=0.6$ @ $Re=9e6$;
- $Cl_{max}=1.82$ that is more than require 1.80;
- Cl_{max} does not changes significantly for transition fixed at 0.05c (top and bottom);
- C_m within normal operating range is less than for the competing airfoils;
- smooth stall shall be demonstrated by additional simulation/analysis/tests.

References

1. NASA TP 1865 "Design and Experimental Results for Flapped NLF Airfoil"
2. XFOIL 6.96 User Guide

	Project	Document Name	Document No.	Page
	-	XFOIL Results for NLF(1)-0215M Airfoil	NC00.00.00.003	14